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Thermoacoustic instabilities

Prof Aimee S. Morgans Department of Mechanical Engineering

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Acoustic excitation of flames



• Acoustic waves cause flame unsteadiness

Movie by Daniel Durox, EM2C Lab, Centrale Supelec, Paris

Flame unsteadiness generates acoustic waves



• Unsteady flames generate new sound waves



From Talei et al, Theoretical and Computational Fluid Dynamics, 2014

Acoustic excitation of a flame in London free space



Acoustic excitation of enclosed flame

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Possibility for successively growing oscillation amplitudes → Thermoacoustic instability (AKA combustion instability)

Thermoacoustic instability in a Rijke tube

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Quartz tube, open at both ends with a Bunsen flame inside

Thermoacoustic instability in gas turbines

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Gas turbine combustors:

NO_x emissions a major air quality issue

Low $NO_x \rightarrow$ lean premixed combustion \rightarrow combustion instability







Thermoacoustic instability in gas turbines

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Gas turbine combustors:

NO_x emissions a major air quality issue

Low $NO_x \rightarrow$ lean premixed combustion \rightarrow combustion instability





(Top) Burner assembly before and after combustion instability (Goy et al. 2005) (Left) Turbine blade damage caused by combustion instability

Gas turbines in a low carbon future

• Combustion of hydrogen / ammonia generated as by-products from renewable energy. These also suffer from combustion instability.

From Siemens 'Green' ammonia leaflet, https://www.siemens.co.uk/pool/insights/siemens-green-ammonia.pdf

Nitrogen is a harmless odourless gas that makes up 78% of the air around us.

Hydrogen is the most abundant element in the universe. There are 2 hydrogen atoms in every molecule of **water**.



By using water electrolysis and renewable electricity, ammonia production can be made completely carbon-free. By switching to renewable electricity to make ammonia we could save over 40 million tons of CO2 each year in Europe alone, or over 360 million tons worldwide. We can also burn ammonia to make electricity when the wind is not blowing.

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Gas turbine thermoacoustic instability London

- Combustion instability still can't be reliably predicted...
- Why can't we use computational fluid dynamics?
 Range of length/time scales very large (long acoustic wavelengths versus tiny chemical reaction and turbulent lengths)
- What about experiments?
 - annular geometries, multiple burners
 - high temperatures and pressures
 - TRL5: Millions of £ spent



Thermoacoustic instability analysis and prediction

• Multi-scale treatment



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Linear treatment of acoustic waves



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$$\frac{p'}{\overline{p}} \gg \left(\frac{p'}{\overline{p}}\right)^2 \qquad \qquad \frac{\rho'}{\overline{\rho}} \gg \left(\frac{\rho'}{\overline{\rho}}\right)^2$$

Linear treatment of acoustic waves

Two options:

 Assume zero mean flow (but allow complex geometry and mean temperature field) → HELMHOLTZ SOLVER (e.g. COMSOL, AVSP)

$$\frac{1}{\overline{c}^2}\frac{\partial^2 p'}{\partial t^2} = \frac{\partial^2 p'}{\partial x_i^2}$$

solve stationary wave equation in frequency domain

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 Account for mean flow (but use network of simple geometry modules) → LOW ORDER NETWORK APPROACH (e.g.OSCILOS, LOTAN)

$$\frac{1}{\bar{c}^2}\frac{\bar{D}^2p'}{Dt^2} - \nabla^2 p' = 0$$

solve convected wave equation assuming low spatial-dimension

Low order network approach

• Linear and with low spatial dimension (due to low frequency):



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Movie from Dr Matthew Wright, ISVR, University of Southampton

• Acoustic waves satisfy convected wave equation: $\frac{1}{\bar{c}^2} \frac{D^2 p'}{Dt^2} - \nabla^2 p' = 0$



$$p(x,t) = \bar{p} + A(t - \frac{x}{\bar{c} + \bar{u}}) + B(t + \frac{x}{\bar{c} - \bar{u}})$$

Low order network approach

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- Network of geometry modules with 1-D acoustic waves
- Acoustic boundary conditions at inlet/outlet.
- Linearised flow conservation eqns at junctions and across flame



Acoustic treatment of flame

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• Flame short compared to acoustic wavelengths



Fluctuating heat release rate affects acoustic wave strengths either side of flame



Flame models

• Flame model describes response of Q' to acoustic velocity just ahead of flame



• Linear flame models can be used to predict "modes" (frequency and growth rate) of combustor, but not limit cycle behaviour



➔ Need modelling framework for nonlinear flame models

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The Flame Transfer Function

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The Flame Describing Function



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The Flame Describing Function

$$\frac{\hat{Q}(s)}{\overline{Q}} = H\left(s, \frac{\hat{u}_1(s)}{\overline{u}_1}\right) \frac{\hat{u}_1(s)}{\overline{u}_1}$$



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Procedure for FDF (experimental or numerical):

- Apply harmonic velocity forcing upstream of flame across different frequencies and forcing amplitudes
- After transients have died away, measure gain and phase shift for each frequency/amplitude level.

Coupled predictions with linear flame models

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Modal frequencies, growth rate and modeshapes



Coupled predictions with nonlinear flame models

1.05



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Fully computational prediction of thermoacoustic instability?

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Laboratory combustor:

- Partially premixed turbulent flame combustor
- End combustor or flame 'enclosure' can be short or long



*Balachandran PhD thesis 2005

FDF from reacting flow simulations

Incompressible LES using Open Source CFD code OpenFOAM (ReactingFOAM, one-step chemistry, PaSR for turbulence-combustion interaction, WALE SGS)

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Equiv ratio ϕ = 0.55, flame response to velocity forcing at 160Hz (A=0.65)*#



*Han, Li & Morgans, Combustion & Flame 2015

FDF from reacting flow simulations

1-step chemistry, partially-stirred reactor model for turbulence-chemistry interaction

Full LES flame describing function φ=0.61

Fitting done within OSCILOS*



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*Han, Li & Morgans, Combustion & Flame 2015

Low order simplified network

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OSCILOS module geometry

Closed inlet and open outlet boundary conditions:





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Coupled low order prediction of limit cycle oscillations

	Experiments	Low order prediction*
Instability frequency (Hz)	348	343
Instability amplitude (normalised velocity before flame)	0.21	0.26

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Now more complex combustion rigs...



Open questions on reduced chemistry, turbulence-combustion interaction models, spray flames

Indirect combustion noise (entropy Imperial College London noise)

Entropy noise is one (of two) components of combustion noise



- Acoustic waves which propagate within the combustor.
- Entropy waves (hot/cold spots) which are "swept" downstream, advecting with the flow. In a non-accelerating flow they are "silent".

Indirect combustion noise (entropy noise)

- Q: If entropy waves are silent, what is "entropy noise"?
- A: When the flow is accelerated, acoustic, entropy and vorticity waves all become coupled. Thus by accelerating entropy waves, new acoustic waves are generated*.



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Entropy noise in gas turbines

- Q: Are entropy waves accelerated in real combustion systems?
- A: Yes! In a gas turbine, the flow undergoes rapid acceleration through the combustor exit and first turbine stage. The entropy waves then generate "entropy noise".





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Stator exit shock waves from Mee et al. (1992)

Thermoacoustic instability in the UK Cardiff GTRC facility

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- Experimental facilities set-up for thermoacoustic analysis at: Loughborough, Cardiff, Cambridge, UCL, Imperial **College London**
- Simulations supported through UKCTRF (ARCHER)
- Current EPSRC support:
 - CHAMBER grant (Imperial/UCL)
 - Flex-E-Plant (Loughborough + many others)
 - ARCHER through the UKCTRF
 - A few PhDs through Imperial CDT, Cambridge/Loughborough CDT
 - Co-funding from industry (Rolls-Royce UTCs, Siemens)





Imperial College Thermoacoustic instability in the UK London

A few ideas for future collaboration:

- Predicting instability in more industrially-relevant experiments (need lots of thermoacoustic characterisation: boundary conditions, flame describing function, mean temperature profile)
- Multiple interacting flames or burners
- Transverse modes (challenging for acoustic modelling and flame modelling)
- Hydrogen/ammonia combustion
- Distributed propulsion on aeroplanes (Aerospace Technology Institute)
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